### **Nuclear and Particle Physics**

## Barem

i)The Heisenberg Uncertainty Principle relates the uncertainties  $\Delta E$  in energy and  $\Delta t$  in time by:

$$\Delta E \Delta t \ge \frac{h}{4\pi}$$

 $d \approx c\Delta t$ , where *c* is the speed of light as the maximum value hypothetical possible.

$$\Delta t \approx \frac{d}{c} = \frac{10^{-15} m}{3 \times 10^8 m/sec} \approx 3.3 \times 10^{-24} sec$$

$$\Delta E \approx \frac{h}{4\pi\Delta t} = \frac{6.63 \times 10^{-34} Jsec}{4 \times 3.14 \times 3.3 \times 10^{-24} sec} = 1.6 \times 10^{-11} J = 1.6 \times 10^{-11} J \times \frac{1 MeV}{1.6 \times 10^{-13} J} = 100 MeV$$

$$\Delta E = mc^2 \text{ and thus } m_{\pi} = \frac{\Delta E}{c^2} = 100 MeV/c^2.$$
Punctaj: 2p

**Punctaj:** 

ii) The pion must then be captured and, thus, cannot be directly observed because that would amount to a permanent violation of mass-energy conservation. Such particles (like the pion it is a virtual particle, because they cannot be directly observed but their *effects* can be directly observed.)

# **Punctaj:**

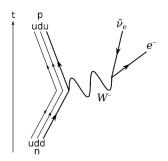
1p

iii) The correct result and numerical value is: 
$$E_K = \frac{(m_p + m_n + m_\pi)^2 c^2 - (m_p + m_n)^2 c^2}{2m_n} \approx 280 \, MeV$$

## **Punctaj:**

2р

iv)



# Punctaj:

2p

v) What was the dominant interaction (force) in this case. Calculate the radius of action of this interaction in the considered disintegration.

$$\Delta E \,\Delta t \geq \frac{h}{4 \,\pi}$$

$$x \approx c \Delta t = \frac{h}{4 \pi \Delta E} = \frac{h}{4 \pi m c^2} = \frac{3 \times 10^8 \frac{m}{sec} \times 6,63 \times 10^{-34} Jsec}{4 \times 3,14 \times \frac{83 \, GeV}{c^2} \times c^2 \times 1,6 \times 10^{-10} \frac{J}{GeV}} = 1,2 \times 10^{-18} m$$
Punctaj:
Oficiu:

Total:

10p

# Thermodynamics

1. The state equation of a thermodynamic system is:

$$p = \frac{AT^3}{V}$$

in which p, V and T represent pressure, volume and temperature, whereas A is a constant. The expression of the internal energy of the system is provided by the relation:

$$U = BT^n \ln\left(\frac{V}{V_0}\right) + f(T)$$

in which B, n and V<sub>0</sub> are constants, whereas f(T) is a function which depends only on temperature. Find the values of B and n.

## **Solution**

From the fundamental equation of thermodynamics, one obtains:

(1) 
$$dS = \frac{dU}{T} + \frac{pdV}{T}$$

U is function of state and has total exact differential:

(2) 
$$U(T,V) = \left(\frac{\partial U}{\partial T}\right)_V dT + \left(\frac{\partial U}{\partial V}\right)_T dV$$

(3) 
$$\left(\frac{\partial U}{\partial T}\right)_V = nBT^{n-1}ln\left(\frac{V}{V_0}\right) + \left(\frac{\partial f}{\partial T}\right)_V$$

(4) 
$$\left(\frac{\partial U}{\partial V}\right)_T = B \frac{T^n}{V}$$

From the given equation of state:

(5) 
$$\frac{p}{T} = \frac{AT^2}{V}$$

From (1), (3), (4) and (5), one obtains:

(6) 
$$dS = \left[\frac{1}{T}\left(nBT^{n-1}ln\left(\frac{V}{V_0}\right) + \left(\frac{\partial f}{\partial T}\right)_V\right)\right]dT + \left[\frac{1}{T}\frac{BT^n}{V} + \frac{AT^2}{V}\right]dV$$

(7) 
$$dS = \left[ nBT^{n-2}ln\left(\frac{V}{V_0}\right) + \frac{1}{T}\left(\frac{\partial f}{\partial T}\right)_V \right] dT + \left[\frac{BT^{n-1} + AT^2}{V}\right] dV$$

S is function of state (S=S(T,V)) and therefore the following relations hold:

(8) 
$$S(T,V) = \left(\frac{\partial S}{\partial T}\right)_V dT + \left(\frac{\partial S}{\partial V}\right)_T dV$$

(9) 
$$\frac{\partial^2 S}{\partial V \partial T} = \frac{\partial^2 S}{\partial T \partial V}$$

From (7), (8) and (9) one obtains:

(10) 
$$\frac{\partial \left(nBT^{n-2}ln\left(\frac{V}{V_0}\right) + \frac{1}{T}\left(\frac{\partial f}{\partial T}\right)_V\right)}{\partial V} = \frac{\partial \left(\frac{BT^{n-1} + AT^2}{V}\right)}{\partial T}$$

$$BT^{n-2} = 2AT$$

Therefore:

# Electricity and Magnetism Grading

Ex officio: 1point

The flux density B(x) in a close region of x-axis is

$$B(x) \simeq \frac{\mu_0 I}{2R} \frac{1}{\left[1 + (x/R)^2\right]^{3/2}},$$
 0.5p

where x = 0 is the center of the circular coil.

For small radial deviations r << R,  $B(x, r) \cong B(x)$  and the magnetic flux through the crosscircular area  $\pi r^2$  is given by the loop integral  $\int \mathbf{A} \cdot \mathbf{d} \mathbf{l}$  of the magnetic vector potential  $\mathbf{A}$ . Since the contribution to this loop integral is only due to the angular component  $A_{\varphi}(x, r)$ , we get

$$A_{\varphi}(x,r) \cong \frac{\mu_0 I R^2}{4} \frac{r}{\left(x^2 + R^2\right)^{3/2}} .$$
 2p

The corresponding angular component  $\Pi_{\varphi}$  of canonical momentum is given by

$$\Pi_{\varphi} \simeq mr^2 \dot{\varphi} - eA_{\varphi}(x,r)r .$$
 **3p**

Noteworthy,  $\Pi_{\varphi}$  is a conserved quantity and since initially **v** is parallel to *x*-axis,  $\Pi_{\varphi} = 0$  (as follows from  $A_{\varphi}(x,r) \to 0$  for  $x \to \pm \infty$ ). Therefore, we get

$$mr\dot{\varphi} \cong eA_{\varphi}(r),$$
 1p

$$\dot{\varphi} \simeq \frac{eA_{\varphi}(r)}{mr} = \frac{\mu_0 eIR^2}{4m} \frac{1}{\left(x^2 + R^2\right)^{\beta/2}} = \frac{d\varphi}{dx} \cdot \frac{dx}{dt} \simeq \frac{d\varphi}{dx} v, \qquad \mathbf{1p}$$

$$d\varphi \simeq \frac{\mu_0 e I R^2}{4 m v} \frac{1}{(x^2 + R^2)^{3/2}} dx$$
 . **0.5p**

Long after passing through the coil, the electron will have rotated around *x*-axis with an angle  $\varphi(I, v)$  given by the fair approximation

$$\varphi \simeq \frac{\mu_0 e I R^2}{4 m v} \int_{-\infty}^{+\infty} \frac{1}{(x^2 + R^2)^{p/2}} dx = \frac{\mu_0 e I}{2 m v}.$$
 **1p**

### Total: 10 points

<u>Note</u>: There is also a less elegant method to approach the problem. In essence, it proceeds as follows:

$$B_x(x+dx,r=0) - B_x(x,r=0) = \left(\frac{dB_x}{dx}\right) dx$$

The infinitesimal flux through a closed cylindrical surface centered on x-axis, with length dx and radius r << R, is  $d\Phi \simeq \pi r^2 [B_x(x+dx) - B_x(x)] - 2\pi r B_r(x,r) dx$ . Since div **B** =0,  $d\Phi =0$ , hence

$$r\left(\frac{dB_x}{dx}\right) \approx 2B_r(x,r),$$
$$-\frac{3\mu_0 IR^2}{2}rx\left(x^2 + R^2\right)^{5/2} = 2B_r(x,r).$$

The Lorentz force acting on electron is

$$F_{\varphi} = evB_r(x,r),$$

or

$$F_{\varphi} = \frac{d}{dt}(mv_{\varphi}) = \frac{d}{dt}(m\dot{\varphi}r) = \frac{3\mu_0 e IR^2 v}{4} \frac{rx}{\left(x^2 + R^2\right)^{5/2}}.$$

Therefore, with dx = vdt, we get the same equation as before.

$$\dot{\varphi} \simeq \frac{eA_{\varphi}(r)}{mr} = \frac{\mu_0 eIR^2}{4m} \frac{1}{\left(x^2 + R^2\right)^{3/2}}, \ \varphi \simeq \frac{\mu_0 eI}{2mv}$$

Regardless of the method used, the students received the appropriate score.

# **Optică** - Barem

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A. The constructive interference condition for  $\lambda'=640$  nm is given by:

$$2 n l \cos \theta_r + \frac{\lambda'}{2} = m' \lambda' \qquad 0.25 \text{ p}$$

while the destructive interference condition for  $\lambda''=400$  nm is given by:

$$2 n l \cos \theta_r + \frac{\lambda''}{2} = \left( m'' + \frac{1}{2} \right) \lambda'' \qquad 0.25 \text{ p}$$

where m', m'' are positive integer numbers,  $\theta_r$  is the refraction angle for the respective incidence angle  $i=30^\circ$ ,  $sini=nsin \theta_r$ . Considering the refraction law (Snell's law) and rearranging the first two equations may be written as:

$$2l\sqrt{n^2 - \sin^2 i} = \frac{2m' - 1}{2}\lambda'$$

$$2l\sqrt{n^2 - \sin^2 i} = m''\lambda''$$
O.25 p

By combining the two equations, we obtain:

$$\frac{2m''}{2m-1} = \frac{\lambda}{\lambda''} = \frac{8}{5} sau 5m'' = 4(2m'-1)$$
 0.25 p

m''=4m si m'=(5m+1)/2 cu m=1,3,5... The minimum thickness is then obtained for m''=4, m'=3: 0.5 p

$$l = \frac{2\lambda''}{\sqrt{n^2 - \sin^2 i}} l = 0.65 \,\mu m \qquad 0.5 \,\mathrm{p}$$

B. At the air-layer separation surface  $(n_0 - n_1)$ :

$$\begin{cases}
E_o + E_r = E_{1t} + E_{1r} \\
n_o E_o - n_o E_r = n_1 E_{1t} - n_1 E_{1r}
\end{cases} (1)$$
0.5 p

And at the layer-lens separation surface  $(n_1-n)$ :

$$\begin{cases} E_{1t}e^{-ikl} + E_{1r}e^{ikl} = E_t \\ n_1E_{1t}e^{-ikl} - n_1E_{1r}e^{ikl} = nE_t \end{cases} \begin{cases} E_{1t}\frac{n+n_1}{2n_1}E_te^{-ikl} \\ E_{1r} = \frac{n_1 - n}{2n_1}E_te^{-ikl} \end{cases}$$
 0.75 p  
$$\begin{cases} E_o + E_r = \frac{n+n_1}{2n_1}E_te^{-ikl} \\ n_o E_o - n_o E_r = \frac{n+n_1}{2}E_te^{-ikl} - \frac{n_1 - n}{2}E_te^{-ikl} \end{cases}$$

$$\begin{cases} E_o + E_r = \left( coskl + i\frac{n}{n_1} sinkl \right) E_t \\ n_o E_o - n_o E_r = \left( in_1 sinkl + n coskl \right) E_t \end{cases}$$

The reflection coefficient in amplitude can be obtained from the previous equations as:

$$r = \frac{E_r}{E_o} = \frac{n_1(n_o - n) coskl + i (n n_o - n_1^2) sinkl}{n_1(n_o + n) coskl + i (n n_o + n_1^2) sinkl}$$
 0.5 p

The equation of the energy reflection coefficient is then:

$$R = r r^{\Box} = \frac{\left[n_{1}(n_{o} - n) coskl\right]^{2} + \left[\left(n n_{o} - n_{1}^{2}\right) sinkl\right]^{2}}{\left[n_{1}(n_{o} + n) coskl\right]^{2} + \left[\left(n n_{o} + n_{1}^{2}\right) sinkl\right]^{2}}$$
 0.25 p

The layer is anti-reflective, i.e. R=0, if  $nn_0=n_1^2$  and coskl=0,  $kl=\pi/2$ : 0.5 p

$$n_1 = \sqrt{n} = 1.22$$
 0.25 p

$$l = \frac{\lambda_1}{4} = \frac{\lambda_o}{4n_1} = 102nm \qquad 0.25 \text{ p}$$

C. The equations between the incident and the reflected components for two consecutive separating surfaces can be expressed as (1):

Or using matrices as :

$$\begin{pmatrix} E_o + E_r \\ n_o E_o - n_o E_r \end{pmatrix} = \begin{pmatrix} \cos kl & \frac{i}{n_1} \sin kl \\ i n_1 \sin kl & \cos kl \end{pmatrix} \begin{pmatrix} E_{1t} + E_{1r} \\ n_1 E_t - n_1 E_{1r} \end{pmatrix} = M \begin{pmatrix} E_{1t} + E_{1r} \\ n_1 E_t - n_1 E_{1r} \end{pmatrix} 0.5 p$$

Where the matrix M is defined for a layer of length l and refractive index n<sub>1</sub>.

$$M = \begin{pmatrix} \cos kl & \frac{i}{n_{1}} \sin kl \\ in_{1} \sin kl & \cos kl \end{pmatrix}$$
$$\begin{pmatrix} E_{o} + E_{r} \\ n_{o} E_{o} - n_{o} E_{r} \end{pmatrix} = \begin{pmatrix} \cos kl & \frac{i}{n_{1}} \sin kl \\ in_{1} \sin kl & \cos kl \end{pmatrix} \begin{pmatrix} E_{t} \\ n E_{t} \end{pmatrix} = \begin{pmatrix} \cos kl & \frac{i}{n_{1}} \sin kl \\ in_{1} \sin kl & \cos kl \end{pmatrix} \begin{pmatrix} E_{t} + 0 \\ n E_{t} - n \times 0 \end{pmatrix}$$

From this, it results that after transversing N thin layers, we can write the following for the electric field components:  $\begin{pmatrix} E_o + E_r \\ n_o E_o - n_o E_r \end{pmatrix} = M_1 M_2 \dots M_N \begin{pmatrix} E_t \\ n E_t \end{pmatrix}$ 0.25 p When depositing 2N layers successively onto the surface of the support substrate n, if we have identical odd layers represented by  $n_1$ ,  $l_1$ , and also identical odd layers represented by  $n_2$ ,  $l_2$ , then a matrix relationship between the electric fields will result as:

$$\begin{pmatrix} E_o + E_r \\ n_o E_o - n_o E_r \end{pmatrix} = M_1 M_2 \dots M_{2N-1} M_{2N} \begin{pmatrix} E_t \\ nE_t \end{pmatrix} = (M_1 M_2)^N \begin{pmatrix} E_t \\ nE_t \end{pmatrix}$$
 0.25 p

Where the matrix:

$$M_{1}M_{2} = \begin{pmatrix} \cos k_{1}l_{1} & \frac{i}{n_{1}}\sin k_{1}l_{1} \\ i n_{1}\sin k_{1}l_{1} & \cos k_{1}l_{1} \end{pmatrix} \begin{pmatrix} \cos k_{2}l_{2} & \frac{i}{n_{2}}\sin k_{2}l_{2} \\ i n_{2}\sin k_{2}l_{2} & \cos k_{2}l_{2} \end{pmatrix}$$

This matrix becomes, in the case of some layers, a quarter wave  $l_1=\lambda_o/4n_1$  ,  $~l_2=\lambda_o/4n_2$  :

$$M_{1}M_{2} = \begin{pmatrix} 0 & \frac{i}{n_{1}} \\ i n_{1} & 0 \end{pmatrix} \begin{pmatrix} 0 & \frac{i}{n_{2}} \\ i n_{2} & 0 \end{pmatrix} = \begin{pmatrix} \frac{-n_{2}}{n_{1}} & 0 \\ 0 & \frac{-n_{1}}{n_{2}} \end{pmatrix}$$

$$0.5 \text{ p}$$

$$\begin{pmatrix} E_{o} + E_{r} \\ n_{o}E_{o} - n_{o}E_{r} \end{pmatrix} = \begin{pmatrix} \left( \frac{-n_{2}}{n_{1}} \right)^{N} & 0 \\ 0 & \left( \frac{-n_{1}}{n_{2}} \right)^{N} \end{pmatrix} \begin{pmatrix} E_{t} \\ nE_{t} \end{pmatrix}$$

The reflection coefficient for a mirror with N double layers is:

$$r = \frac{\left(\frac{n_2}{n_1}\right)^{2N} - \frac{n}{n_o}}{\left(\frac{n_2}{n_1}\right)^{2N} + \frac{n}{n_o}} R = \left(\frac{\left(\frac{n_2}{n_1}\right)^{2N} - \frac{n}{n_o}}{\left(\frac{n_2}{n_1}\right)^{2N} + \frac{n}{n_o}}\right)^2 \qquad 0.5 \text{ p}$$

It is observable that the reflection coefficient's magnitude escalates as the number of layers increases,  $R \rightarrow 1$ .

For N=1 the anti-reflective layer condition is:

$$\left(\frac{n_2}{n_1}\right)^2 = \frac{n}{n_o} \tag{0.5 p}$$

The condition is similar to the one obtained at point b, only this time it is easier to find two materials that have the relative index  $n_{21} = \sqrt{n/n_o}$  than to find a material with this index. 0.5 p

The reflection coefficient for a single titanium dioxide-magnesium fluoride double layer is:

$$R = \left(\frac{n_{21}^{2} - 1}{n_{21}^{2} + 1}\right)^{2} = 25\%$$
 1 p

The number of double layers necessary to obtain a reflection coefficient R is:

$$\left(\frac{n_2}{n_1}\right)^{2N} = \frac{1+\sqrt{R}}{1-\sqrt{R}} N = \frac{1}{2} \frac{lg \frac{1+\sqrt{R}}{1-\sqrt{R}}}{lg \frac{n_2}{n_1}} N = 4 \text{ for } R = 95\%$$
 1 p

PLANCKS - Cardinativity in disordered electronic systems  
- Correction key -  
2.2)  

$$\sum_{\alpha} F_{\alpha} = 2 \vee \int de \ m(e) F(e) , \quad (\forall) F$$

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2.iii):  

$$H = T + V_{a} + V_{b} + V_{ab} = \begin{cases} 141 > 1 \\ 142 > = \frac{1}{\sqrt{2}} (1a > +1b >) & bondury \\ H_{a,b} = T + V_{a,b} & 1 \\ 142 > = \frac{1}{\sqrt{2}} (1a > -1a >) & axta-bondury \\ H_{1}(h) = e_{1}(h) > \\ H_{1}(h) > = e_{1}(h) > \\ H_{1}(h) > = e_{1}(h) > \\ H_{1}(h) > \\ H_{1}(h) > \\ H_{1}(h) > \\ H_{2}(h) > \\ H_{1}(h) > \\ H_{1}(h) > \\ H_{2}(h) > \\ H_{2$$

2. ix)  
Minimum hopping distance: 
$$R \ge R_{\omega}$$
  
 $2I = 2I_{o}e^{-KR_{\omega}} \le t_{\omega} = R_{\omega} = \frac{1}{K} \ln \frac{2I_{o}}{t_{\omega}}$   
if centers too close, I monases exponendially, electron  
hopping lass probable.  
 $\langle \sigma(\omega) \rangle = \frac{2Re^{2}}{3K} [m(\epsilon_{F})]^{2} (t_{\omega})^{2} \int d\vec{r}_{a} \int d\vec{r} |r_{aF}|^{2}$   
 $|r_{aF}|^{2} = \frac{R^{2}}{4}, \quad R \in (R_{\omega}, R_{\omega} + \frac{1}{K}) \in if$  too large  
distances,  $|r_{aF}| \ll Re^{-KR} \rightarrow 0.$   
 $\Rightarrow \langle \sigma(\omega) \rangle \approx const \cdot \omega^{2} \ln(\frac{t_{\omega}}{2I_{o}})^{4}$   
1 point each item.  $|\Rightarrow| 10 \text{ points}]$ 

1. The average lifetime of the muon in its proper/rest frame is  $2.2 \cdot 10^{-6}s$ , its rest mass is 106 MeV.

(a) Assuming that muons travel at 99.8% of the speed of light, show that cosmic radiation muons can indeed be detected on the surface of the Earth. Take d = 10km as thickness of Earth's atmosphere and 299.8  $\cdot 10^6$ m/s the speed of light. The direction of the muon is vertical with respect to the ground.

(b) What is the smallest energy required for muons to hit the ground before they decay, assuming that they are produced at an altitude of 10 km above ground? (here you drop the velocity assumption at point (a)!). The direction of the muon is vertical again.

(c) A circular accelerator has a radius of 50m. How many turns can a muon take on average in this ring before it decays if its energy is kept constant at 1 GeV? Here, take  $c = 3 \cdot 10^8 m/s$ .

**Solution**. (a) The lifetime  $\tau_0$  is measured in the rest frame of the muon. Due to time dilation, the lifetime in the rest frame of the Earth will be

$$\tau = \tau_0 \gamma(v),$$

where v is the velocity of the muon relative to Earth. [15%]

With v = 0.998c, one obtains

$$\tau = \frac{\tau_0}{\sqrt{1 - \frac{v^2}{c^2}}} \approx 15.8\tau_0.$$

During this time, the muon will move the distance

$$\tau v \approx 15.8 \cdot 2.2 \cdot 10^{-6} \cdot 0.998 \cdot 299.8 \cdot 10^{6} \text{ m} \approx 10.4 \text{ km}$$

which is bigger than the thickness of Earth's atmosphere explaining the detection. [15%] (b) The muon must travel the distance d = 10 km in the time  $\tau$ , which is the time dilated mean life  $\tau_0$  of the muon in its rest frame. It follows that

$$d \leqslant v\tau = v\gamma(v)\tau_0.$$

The velocity of the muon is given by  $v = pc^2/E$ , and thus, we have

$$\gamma(v) = \frac{1}{\sqrt{1 - (v/c)^2}} = \frac{E}{\sqrt{E^2 - p^2 c^2}} = \frac{E}{mc^2}$$

Inserting this into the above inequality, we obtain

$$d \le \frac{pc}{mc^2} c\tau_0.$$

Inserting the numerical values, we find that  $pc \gtrsim 15mc^2 \simeq 1.6$ GeV, and thus, it holds that  $E \simeq pc \gtrsim 1.6$ GeV. [25%]

(c) A time interval for a muon and a time interval for an observer in the lab frame are related through the time dilation formula

$$\gamma(v)d\tau = dt,$$

where  $d\tau$  is the time interval for the muon, dt is the time interval for the observer n the lab frame, and v is the muon velocity. The muon velocity is constant (since he total energy is constant) and given by

$$v = \frac{p}{E} = \frac{\sqrt{E^2 - m^2}}{E} = \sqrt{1 - \frac{m^2}{E^2}}$$

where p is the muon momentum, E is the muon energy, and m is the muon mass.

[15%]

It follows that

$$\gamma(v) = \frac{E}{m},$$

and thus, we obtain

$$t = \frac{E}{m}\tau = \frac{1 \text{GeV}}{106 \text{MeV}}\tau \simeq 9.5\tau.$$

The average lifetime of the muon in the lab frame is therefore  $21\mu$ s. Since  $\gamma(v)$  is known we determine  $v/c \approx 0.995$ , so the length travelled by the muon in the lab frame in the average lifetime is given by

$$\ell = vt \approx 0.995 \cdot ct \approx 0.995 \cdot 3 \cdot 10^8 \text{ m/s} \cdot 21 \cdot 10^{-6} \text{ s} = 6270 \text{ m}.$$

## [15%]

The circumference of the circular accelerator is given by

$$L = 2\pi r \simeq 300$$
 m.

Thus, the average number of turns taken by a muon is given by

$$N = \frac{\ell}{L} \simeq 21.$$

[15%]

# How cold is too cold?

Since the latent heat of ice is given, the skating process has to be modelled as a first order phase transition. This implies that (phase 1 is water, phase 2 is ice in what follows)

(2p) 
$$\mu_1 = \mu_2 \to d\mu_1 = d\mu_2.$$
 (1)

The chemical potential is also the reduced Gibbs potential, so

(1p) 
$$-S_1 dT_1 + V_1 dp_1 = -S_2 dT_2 + V_2 dp_2.$$
 (2)

The two phases are in thermal, chemical and mechanical equilibrium (by definition of a first order phase transition). This is expressed mathematically as

(1p) 
$$p_1 = p_2 = p, \qquad T_1 = T_2 = T,$$
 (3)

together with relation (1). Inserting (3) into (2) we obtain the Clausius-Clapeyron equation on the phase line

(1p) 
$$\left(\frac{dp}{dT}\right)_{\text{phase line}} = \frac{S_2 - S_1}{V_2 - V_1}.$$
 (4)

Moreover, at temperatures higher than those of phase transitions  $\mu_1 ; \mu_2$  and at temperatures lower than those of phase transition  $\mu_1 ; \mu_2$ . In other words, there's no ice above the freezing point and no water below the freezing point. This implies that

(1p) 
$$\left(\frac{\partial \mu_1}{\partial T}\right) < \left(\frac{\partial \mu_2}{\partial T}\right),$$
 (5)

i.e., for any temperature,  $S_1 > S_2$ .

The lowest temperature permitted for enjoyable skating is the temperature at which the pressure on the coexistence line is equal to the pressure exerted by the skater on ice. For a skater of normal weight and a reasonable skating blade of sides 30 cm (to simplify calculations) by 1 mm, the pressure exerted by the skater is  $p' \simeq 13$  atm (two blades per normal human). The specific volume of ice is larger than the specific volume of water, Using the pressure and temperature at the freezing point of water we obtain

(3p) 
$$\frac{p'-p_0}{T_{\min}-T_0} = -\frac{h}{T_{\min}\Delta V},$$
 (6)

which can be inverted to obtain

(1p) 
$$T_{\min} = \frac{T_0}{1 + \frac{(p' - p_0)\Delta V}{h}} \simeq -0.09^o \text{ C}$$
 (7)

### Solution Neutrons in a box

a)

- the average time  $<t>=<D>/v=<D>/\sqrt{2 * E/m}$  (1p)
- the average distance travelled by a neutron before tunneling through a wall is
- $< D >= d * T + 3 * d * R * T + 5 * d * R^2 * T + \dots = d * (1 + 3 * R + 5 * R^2 + \dots) * T (1p)$

♦  $< D >= d * (R + 1) * T/(1 - R)^2 = d * (R + 1)/T$  (0.5p)

♦  $< t >= d * (R + 1) / (T * \sqrt{2 * E/m}) (0.5p)$ 

b)

- \* the number of neutrinos that tunnel through the walls in a unit of time is equal to  $N/\langle t \rangle$  (1p)
- ✤ equilibrium is reached when P = N < t >, thus  $N = P * < t > = P * d * (R + 1) / (T * <math>\sqrt{2 * E/m})$  (1p)

c)

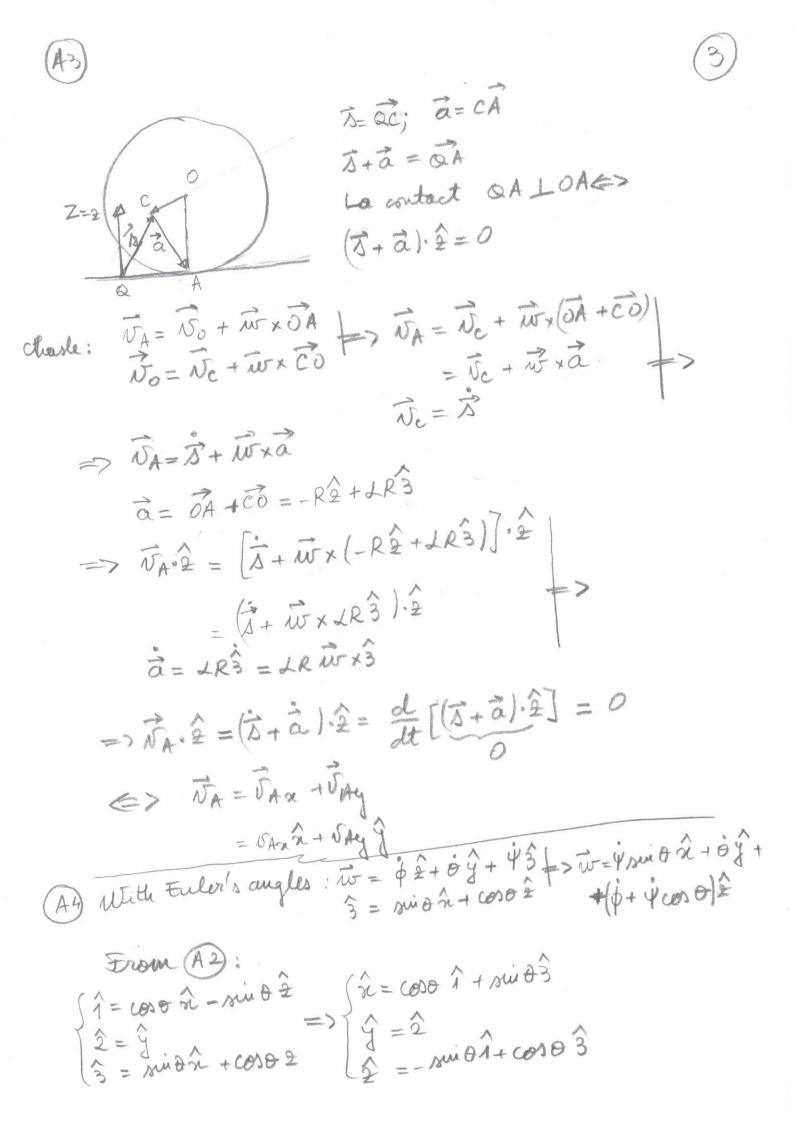
- $\clubsuit$  write the Schrodinger equation for the three sectors of the potential barrier (0.5p)
- solve all the three Schrodinger equations (1p)
- $\diamond$  impose the continuity of the wave-function and of its first derivative (0.5p)
- ✤ solve the system of equation produced by the continuity conditions (1p)

d)

- calculate the currents of probability (1p)
- calculate the transmission and reflection coefficient (1p)

Lipps 2024 A1 side view Ff 1 VG  $\vec{F} = m \vec{a}_c = (N - mq) \vec{a} + \vec{F} \vec{p} =$ = (N-mg) - Man in Not c'has a complexe motion, there are external forces which make āc 70. The principal and central asces, that is, the Euler's system 123, because re E + W + 1cw = CA + (N+ Fg) becomes 1= ( 000) and simpler.

$$\begin{array}{l} \left( \begin{array}{c} A \\ z \end{array} \right) \\ \hline F_{end} &= \overline{cA} \times \left( A \right) \stackrel{2}{\mp} + \overline{f_{f}} \right) = \overline{a} \times \left( N \stackrel{2}{\oplus} + \overline{f_{f}} \right) \\ \hline a = \overline{cA} = \overline{co} + \overline{oA} = \mathcal{A} \stackrel{2}{\Rightarrow} - R \stackrel{2}{\Rightarrow} \\ \hline a = \overline{cA} = \overline{co} + \overline{oA} = \mathcal{A} \stackrel{2}{\Rightarrow} - R \stackrel{2}{\Rightarrow} \\ \hline a = \overline{cA} = \overline{co} + \overline{oA} = \mathcal{A} \stackrel{2}{\Rightarrow} - R \stackrel{2}{\Rightarrow} \\ \hline a = \overline{cA} = \overline{co} + \overline{oA} = \mathcal{A} \stackrel{2}{\Rightarrow} - R \stackrel{2}{\Rightarrow} \\ \hline a = \left( \begin{array}{c} con \Theta & 0 & -nui \Theta \\ 0 & 1 & 0 \\ nui \Theta & 0 & co \sigma \end{array} \right) \left( \begin{array}{c} \mathcal{A} \\ \mathcal{A} \end{array} \right) = \\ \hline \mathcal{A} \\ \hline \mathcal{A} \end{array} \right) \\ = \left( \begin{array}{c} con \Theta \stackrel{2}{\Rightarrow} - nui \Theta \stackrel{2}{\Rightarrow} \\ nui \Theta \stackrel{2}{\Rightarrow} - nui \Theta \stackrel{2}{\Rightarrow} \end{array} \right) \\ \hline \mathcal{R} \stackrel{1}{\Rightarrow} \\ = \left( \begin{array}{c} con \Theta \stackrel{2}{\Rightarrow} - nui \Theta \stackrel{2}{\Rightarrow} \\ nui \Theta \stackrel{2}{\Rightarrow} - nui \Theta \stackrel{2}{\Rightarrow} \end{array} \right) \\ \hline \mathcal{R} \stackrel{1}{\Rightarrow} \\ = \mathcal{A} \stackrel{2}{=} \left( \begin{array}{c} con \Theta \stackrel{2}{\Rightarrow} - nui \Theta \stackrel{2}{\Rightarrow} + \overline{f_{f}} \stackrel{2}{\Rightarrow} \right) \\ = \mathcal{A} \stackrel{2}{=} \left( \begin{array}{c} A \stackrel{2}{\Rightarrow} \stackrel{2}{\Rightarrow} \stackrel{2}{\Rightarrow} \right) \times \left( N \stackrel{2}{\Rightarrow} + \overline{f_{f}} \stackrel{2}{\Rightarrow} \stackrel{2}{\Rightarrow} \right) \\ = \mathcal{A} \stackrel{2}{=} \left( \begin{array}{c} A \stackrel{2}{\Rightarrow} \stackrel{2}{\Rightarrow} \stackrel{2}{\Rightarrow} \right) \times \left( N \stackrel{2}{\Rightarrow} + \overline{f_{f}} \stackrel{2}{\Rightarrow} \stackrel{2}{\Rightarrow} \right) \\ = \mathcal{A} \stackrel{2}{=} \left( \begin{array}{c} A \stackrel{2}{\Rightarrow} \stackrel{2}{\Rightarrow} \stackrel{2}{\Rightarrow} \right) \times \left( N \stackrel{2}{\Rightarrow} \stackrel{2}{\Rightarrow} \right) \\ = \mathcal{A} \stackrel{2}{=} \left( \begin{array}{c} A \stackrel{2}{\Rightarrow} \stackrel{2}{\Rightarrow} \stackrel{2}{\Rightarrow} \right) \times \left( N \stackrel{2}{\Rightarrow} \stackrel{2}{\Rightarrow} \right) \\ = \mathcal{A} \stackrel{2}{=} \left( \begin{array}{c} A \stackrel{2}{\Rightarrow} \stackrel{2}{\Rightarrow} \right) \times \left( N \stackrel{2}{\Rightarrow} \stackrel{2}{\Rightarrow} \right) \\ = \mathcal{A} \stackrel{2}{=} \left( \begin{array}{c} A \stackrel{2}{\Rightarrow} \stackrel{2}{\Rightarrow} \right) \times \left( N \stackrel{2}{\Rightarrow} \stackrel{2}{\Rightarrow} \right) \\ = \mathcal{A} \stackrel{2}{=} \left( \begin{array}{c} A \stackrel{2}{\Rightarrow} \stackrel{2}{\Rightarrow} \stackrel{2}{\Rightarrow} \right) \times \left( \begin{array}{c} A \stackrel{2}{\Rightarrow} \stackrel{2}{\Rightarrow} \right) \\ = \mathcal{A} \stackrel{2}{=} \left( \begin{array}{c} A \stackrel{2}{\Rightarrow} \stackrel{2}{\Rightarrow} \stackrel{2}{\Rightarrow} \right) \\ = \mathcal{A} \stackrel{2}{=} \left( \begin{array}{c} A \stackrel{2}{\Rightarrow} \stackrel{2}{\Rightarrow} \stackrel{2}{\Rightarrow} \right) \times \left( \begin{array}{c} A \stackrel{2}{\Rightarrow} \stackrel{2}{\Rightarrow} \stackrel{2}{\Rightarrow} \stackrel{2}{\Rightarrow} \right) \\ = \mathcal{A} \stackrel{2}{=} \left( \begin{array}{c} A \stackrel{2}{\Rightarrow} \stackrel{2}{\Rightarrow} \stackrel{2}{\Rightarrow} \right) \\ = \mathcal{A} \stackrel{2}{=} \left( \begin{array}{c} A \stackrel{2}{\Rightarrow} \stackrel{2}{\Rightarrow} \stackrel{2}{\Rightarrow} \right) \\ = \mathcal{A} \stackrel{2}{=} \left( \begin{array}{c} A \stackrel{2}{\Rightarrow} \stackrel{2}{\Rightarrow} \stackrel{2}{\Rightarrow} \right) \\ = \mathcal{A} \stackrel{2}{=} \left( \begin{array}{c} A \stackrel{2}{\Rightarrow} \stackrel{2}{\Rightarrow} \stackrel{2}{\Rightarrow} \stackrel{2}{\Rightarrow} \stackrel{2}{\Rightarrow} \stackrel{2}{\Rightarrow} \stackrel{2}{\Rightarrow} \stackrel{2}{\Rightarrow} \\ = \mathcal{A} \stackrel{2}{=} \left( \begin{array}{c} A \stackrel{2}{\Rightarrow} \stackrel{$$



$$= \sum_{k=1}^{n} \overline{W} = \frac{1}{2} \lim_{k \to 0} \frac{1}{2} (1 - 1) \lim_{k \to 0} \frac{1}{2} + (\frac{1}{2} + \frac{1}{2} + \frac{1}{2} + \frac{1}{2} + (\frac{1}{2} + \frac{1}{2} + \frac{1$$

$$= \frac{1}{\sqrt{3}} = \frac{1}{\sqrt{3}} - (\frac{2}{\sqrt{9}} + \frac{2}{\sqrt{9}} + \frac{3}{\sqrt{9}} + \frac{3}{\sqrt{9}}) \times (\frac{4}{\sqrt{3}} - \frac{2}{\sqrt{2}})$$

$$= \frac{1}{\sqrt{3}} - \frac{1}{\sqrt{3}} + \frac{1}{\sqrt{9}} + \frac{1}{\sqrt{9$$

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=> 
$$E_{T} = K + U_{6} =$$
  
=  $\frac{1}{2} \left[ i_{1} (\dot{\phi} \times \dot{w} + \dot{\sigma} + \dot{\sigma}^{2}) + i_{3} (\dot{\psi} + \dot{\phi} \cos \theta)^{2} \right]$   
+  $\frac{W}{2} \left[ (\int_{\infty} + \dot{\sigma} R (I - L \cos \theta) \right]^{2} + \left[ (\int_{\infty} + \dot{\sigma} R (I - L \cos \theta) \right]^{2} + \left[ (\int_{\infty} + \dot{\sigma} R (I - L \cos \theta) \right]^{2} + \left[ (\int_{\infty} + \dot{\sigma}^{2} L^{2} R^{2} R \sin \theta) \right]^{2} + W_{3} R (I - L \cos \theta).$   
+  $\dot{\sigma}^{2} L^{2} R^{2} R \sin \theta \right]^{2} + W_{3} R (I - L \cos \theta).$ 

(AG) 
$$\vec{L} \cdot \hat{q} = \vec{t} \cdot \hat{q}$$
  
With  $\vec{t} = \vec{t} \cdot \vec{t}$  from (A2) =>  
 $\vec{L} \cdot \hat{q} = \angle R \vec{t} \vec{q}$  suitor

$$\begin{array}{l} \widehat{(A)} \widehat{(L)} = \widehat{(I)} \widehat{(U)} = \left( \begin{array}{c} \widehat{(I)} & 0 & 0 \\ 0 & 1_2 & 0 \\ 0 & 0 & 1_3 \end{array} \right) \left( \begin{array}{c} \widehat{(W_1)} \\ \widehat{(W_2)} \\ \widehat{(W_2)} = \left( \begin{array}{c} \widehat{(I)} \widehat{(W_1)} \\ 1_2 \widehat{(W_2)} \\ 1_3 \widehat{(W_2)} \end{array} \right) = \left( \begin{array}{c} \widehat{(I)} \widehat{(W_1)} \\ 1_2 \widehat{(W_2)} \\ 1_3 \widehat{(W_2)} \end{array} \right) \\ \widehat{(I)} = \left( \begin{array}{c} \widehat{(I)} \widehat{(W_1)} \\ 1_2 \widehat{(W_2)} \\ 1_3 \widehat{(W_2)} \end{array} \right) \\ \widehat{(I)} = \left( \begin{array}{c} \widehat{(I)} \widehat{(W_1)} \\ 1_2 \widehat{(W_2)} \\ 1_3 \widehat{(W_2)} \end{array} \right) \\ \widehat{(I)} = \left( \begin{array}{c} \widehat{(I)} \widehat{(W_1)} \\ 1_2 \widehat{(W_2)} \\ 1_3 \widehat{(W_2)} \end{array} \right) \\ \widehat{(I)} = \left( \begin{array}{c} \widehat{(I)} \widehat{(W_1)} \\ 1_2 \widehat{(W_2)} \\ 1_3 \widehat{(W_2)} \end{array} \right) \\ \widehat{(I)} = \left( \begin{array}{c} \widehat{(I)} \widehat{(W_1)} \\ 1_2 \widehat{(W_2)} \\ 1_3 \widehat{(W_2)} \end{array} \right) \\ \widehat{(I)} = \left( \begin{array}{c} \widehat{(I)} \widehat{(W_1)} \\ 1_2 \widehat{(W_2)} \\ 1_3 \widehat{(W_2)} \end{array} \right) \\ = \left( \begin{array}{c} \widehat{(I)} \widehat{(W_1)} \\ 1_2 \widehat{(W_2)} \\ 1_3 \widehat{(W_2)} \end{array} \right) \\ = \left( \begin{array}{c} \widehat{(I)} \widehat{(W_1)} \\ 1_3 \widehat{(W_2)} \end{array} \right) \\ \widehat{(I)} = \left( \begin{array}{c} \widehat{(I)} \widehat{(W_1)} \\ 1_3 \widehat{(W_2)} \end{array} \right) \\ \widehat{(I)} = \left( \begin{array}{c} \widehat{(I)} \widehat{(W_2)} \\ 1_3 \widehat{(W_2)} \end{array} \right) \\ = \left( \begin{array}{c} \widehat{(I)} \widehat{(W_1)} \\ 1_3 \widehat{(W_2)} \end{array} \right) \\ = \left( \begin{array}{c} \widehat{(I)} \widehat{(W_2)} \\ 1_3 \widehat{(W_2)} \end{array} \right) \\ = \left( \begin{array}{c} \widehat{(I)} \widehat{(W_2)} \\ 1_3 \widehat{(W_2)} \end{array} \right) \\ = \left( \begin{array}{c} \widehat{(I)} \widehat{(W_2)} \\ 1_3 \widehat{(W_2)} \end{array} \right) \\ = \left( \begin{array}{c} \widehat{(I)} \widehat{(W_2)} \\ 1_3 \widehat{(W_2)} \end{array} \right) \\ = \left( \begin{array}{c} \widehat{(I)} \widehat{(W_2)} \\ 1_3 \widehat{(W_2)} \end{array} \right) \\ = \left( \begin{array}{c} \widehat{(I)} \widehat{(W_2)} \\ 1_3 \widehat{(W_2)} \end{array} \right) \\ = \left( \begin{array}{c} \widehat{(I)} \widehat{(W_2)} \\ 1_3 \widehat{(W_2)} \end{array} \right) \\ = \left( \begin{array}{c} \widehat{(I)} \widehat{(W_2)} \\ 1_3 \widehat{(W_2)} \end{array} \right) \\ = \left( \begin{array}{c} \widehat{(I)} \widehat{(W_2)} \\ 1_3 \widehat{(W_2)} \end{array} \right) \\ = \left( \begin{array}{c} \widehat{(I)} \widehat{(W_2)} \\ 1_3 \widehat{(W_2)} \end{array} \right) \\ = \left( \begin{array}{c} \widehat{(I)} \widehat{(W_2)} \\ 1_3 \widehat{(W_2)} \end{array} \right) \\ = \left( \begin{array}{c} \widehat{(I)} \widehat{(W_2)} \\ 1_3 \widehat{(W_2)} \end{array} \right) \\ = \left( \begin{array}{c} \widehat{(I)} \widehat{(W_2)} \\ 1_3 \widehat{(W_2)} \end{array} \right) \\ = \left( \begin{array}{c} \widehat{(I)} \widehat{(W_2)} \\ 1_3 \widehat{(W_2)} \end{array} \right) \\ = \left( \begin{array}{c} \widehat{(I)} \widehat{(W_2)} \\ 1_3 \widehat{(W_2)} \end{array} \right) \\ = \left( \begin{array}{c} \widehat{(I)} \widehat{(W_2)} \\ 1_3 \widehat{(W_2)} \end{array} \right) \\ = \left( \begin{array}{c} \widehat{(I)} \widehat{(W_2)} \\ 1_3 \widehat{(W_2)} \end{array} \right) \\ = \left( \begin{array}{c} \widehat{(I)} \widehat{(W_2)} \end{array} \right) \\ = \left( \begin{array}{c} \widehat{(I)} \widehat{(W_2)} \\ 1_3 \widehat{(W_2)} \end{array} \right) \\ = \left( \begin{array}{c} \widehat{(I)} \widehat{(W_2)} \end{array} \right) \\ = \left( \begin{array}{c} \widehat{(I)} \widehat{(W_2)} \\ 1_3 \widehat{(W_2)} \end{array} \right) \\ = \left( \begin{array}{c} \widehat{(I)} \widehat{(W$$